



# Relation between partial propene oxidation, sulphate content and selective catalytic reduction of NO<sub>x</sub> by propene on ceria/sulphated titania

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## ABSTRACT

The propene catalytic oxidation and the selective catalytic reduction of NO by propene (C<sub>3</sub>H<sub>6</sub>-SCR) have been studied over ceria catalysts supported on sulphated titania (ceria content of 0.9, 0.5, 0.3 and 0.04 wt%). XPS analysis and Raman spectroscopy were carried out in order to obtain information on ceria (oxidation degree, surface content, and particle size) and sulphate compounds (species and surface content). The NO<sub>x</sub> reactivity was mainly linked to the sulphate content. The higher the sulphate content, the higher the NO<sub>x</sub> reactivity. The partial C<sub>3</sub>H<sub>6</sub> oxidation has a role in the NO<sub>x</sub> activity. The lower the partial C<sub>3</sub>H<sub>6</sub> oxidation into CO, the better the NO<sub>x</sub> reactivity. However, N<sub>2</sub> selectivity was higher for the sample with the lowest sulphate content (i.e. the highest partial C<sub>3</sub>H<sub>6</sub> oxidation). Sulphate compounds like SO<sub>3</sub><sup>2−</sup> and/or SO<sub>4</sub><sup>2−</sup> with reduced ceria (Ce<sup>3+</sup>) activate the C<sub>3</sub>H<sub>6</sub> and NO compounds. Moreover, in the range of ceria content studied here, with or without NO in the gas stream, C<sub>3</sub>H<sub>6</sub> oxidation was also related to sulphate content and not to ceria content. Nevertheless, the presence of ceria provides oxygen for NO oxidation to form nitrate, oxygen coming from Ce<sup>3+</sup>Vo species at the surface (Vo: oxygen vacancy). The key parameter between NO<sub>x</sub> reduction and N<sub>2</sub> selectivity was observed to be the sulphate content.

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## 1. Introduction

Many investigations have been conducted on selective catalytic reduction (SCR) of NO into N<sub>2</sub> by hydrocarbons under lean-burn conditions using non-zeolitic oxide and platinum group metal (PGM) catalysts as a potential process for NO<sub>x</sub> emission control [1,2]. The HC-SCR mechanism, involving competition between reduction of NO<sub>x</sub> and reduction of O<sub>2</sub>, in lean conditions, is complex and depends on several parameters: (i) the catalyst formulation [3], (ii) the hydrocarbon [4–7] and (iii) the reaction conditions [8]. A number of reviews on HC-SCR have described several possible mechanisms which may occur during the reaction [9–11,1]. Firstly, a simple mechanism for PGM catalysts using a support with low acidity outlines the dissociation of NO on a reduced metal surface to give N<sub>ad</sub> and O<sub>ad</sub> followed by desorption of N<sub>2</sub> and N<sub>2</sub>O and removal of O<sub>ad</sub> by the reductant. In the case of PGM catalysts deposited on an acidic support, organo-nitro-type species may con-

tribute to the NO<sub>x</sub> reduction activity [12]. An acidic support alone has demonstrated that the reduction of NO occurred due to aldehydes; the reaction was fast and selective at low temperatures [13,14]. Secondly, a bifunctional mechanism has been proposed in which hydrocarbons are converted to carbonyl intermediates that react with NO<sub>x</sub> in an acid-catalysed reaction. The importance of acidity in the reaction has been reported [15–17].

In this work, a tentative of correlation between partial propene oxidation properties, sulphate content and C<sub>3</sub>H<sub>6</sub>-SCR properties of ceria supported on sulphated titania has been carried out.

## 2. Experimental part

### 2.1. Catalyst preparation

The sulphated titania support (theoretical: 2 wt% S) used for catalyst preparation was supplied by Millenium®. Before catalyst preparation, the support was pretreated under air at 500 °C for 2 h. The ceria active phase was deposited at various weight content by impregnation (0.04, 0.3, 0.5, and 0.9 wt%). The ceria acetylacetonate salt precursor (Ce(C<sub>5</sub>H<sub>8</sub>O<sub>2</sub>)<sub>3</sub>) and the sulphated TiO<sub>2</sub> support were introduced in a 250 mL flask and mixed with 50 mL of distilled water. The solution was stirred for 70 min at 70 °C under atmo-

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spheric pressure, then cooled to room temperature under stirring. At the end, the water was evaporated under vacuum at 60 °C in a rotary evaporator. After drying one night under air at 120 °C, the powder was calcined under air at 500 °C for 2 h.

## 2.2. Characterizations

The quantitative measurement of ceria concentration was performed by ICP-OES using a Horiba Jobin Yvon Activa apparatus. The solid sample was previously dissolved by acid. Specific surface areas ( $S_{\text{BET}}$ ) were estimated from  $\text{N}_2$  adsorption at  $-196^\circ\text{C}$  (BET method), using a Tristar Surface Area and Porosity Measurement apparatus from Micromeritics. An Axis Ultra DLD from Kratos Analytical spectrometer equipped with a monochromated Al  $K\alpha$  source ( $h\nu = 1486.6\text{ eV}$ ) was used for the surface analysis. A pressure of  $10^{-7}\text{ Pa}$  was maintained in the chamber during analysis. The analysed area was about ( $300\text{ }\mu\text{m} \times 700\text{ }\mu\text{m}$ ). Surveys, between 0 and 1200 eV, were obtained with constant pass energy of 150 eV, whereas high resolution spectra were recorded at constant pass energy of 40 eV. Powders were pressed onto small indium foils. Charge neutralization was required for all insulating samples. The peaks were referenced to the  $\text{Ti}_{2p3/2}$  line at  $457.7 \pm 0.2\text{ eV}$ , typical for titania powders. Raman measurements were carried out on Horiba Jobin Yvon LabRam HR UV-Vis-NIR spectrometer using green light laser (514 nm). For measurements, the laser was focused on sample analysis area ( $\sim 1\text{ }\mu\text{m}^2$ ). The acquisition time was 20 s.

## 2.3. NOx reduction reactions

The selective catalytic reduction of NOx by  $\text{C}_3\text{H}_6$  ( $\text{C}_3\text{H}_6\text{-SCR}$ ) was carried out in a U-shaped quartz reactor with 200 mg of catalyst. The reactor was electrically heated, with the temperature of the catalyst being monitored using a K-type thermocouple. The reaction mixture was composed of 1100 ppm NO, 1100 ppm  $\text{C}_3\text{H}_6$  and 9%  $\text{O}_2$  in He. The total flow rate was  $120\text{ mL min}^{-1}$  which corresponds to a VVH of about  $35,000\text{ h}^{-1}$ . Reaction products were analyzed by gas chromatography for  $\text{N}_2$ ,  $\text{C}_3\text{H}_6$  and  $\text{CO}_2$  and by IR-UV for NO,  $\text{NO}_2$  and  $\text{N}_2\text{O}$ . The temperature-programmed reaction was started at  $25^\circ\text{C}$ . After stabilization, the catalyst temperature was increased at a rate of  $2^\circ\text{C min}^{-1}$  up to  $500^\circ\text{C}$ . This temperature was maintained 30 min, then decreased to room temperature at a rate of  $1^\circ\text{C min}^{-1}$ . All light-off curves presented in this paper were obtained during the cooling ramp. The conversion of NO into  $\text{N}_2$ , the  $\text{N}_2$  selectivity and the total  $\text{C}_3\text{H}_6$  conversion were calculated by the following Eqs. (1)–(3):

$$X_{\text{NO}-\text{N}_2} = 100 \times \frac{2[\text{N}_2]_t}{[\text{NO}]_{t0}} \quad (1)$$

$$S_{\text{N}_2} = 100 \times \left( \frac{2[\text{N}_2]_t}{2[\text{N}_2]_t + 2[\text{N}_2\text{O}]_t + [\text{NO}_2]_t} \right) \quad (2)$$

$$X_{\text{C}_3\text{H}_6} = 100 \times \left( 1 - \frac{[\text{C}_3\text{H}_6]_t}{[\text{C}_3\text{H}_6]_{t0}} \right) \quad (3)$$

## 2.4. Propene oxidation reactions

Catalytic activity for propene oxidation was measured with a reactant mixture composed of 1100 ppm  $\text{C}_3\text{H}_6$  and 9%  $\text{O}_2$  in He. For each test, 200 mg of catalyst was introduced in a U-shaped quartz reactor. The reactor was electrically heated with the temperature of the catalyst being monitored using a K-type thermocouple. After the reactor was purged under He, a flow rate of  $120\text{ mL min}^{-1}$ , corresponding to a VVH of about  $35,000\text{ h}^{-1}$ , was passed through the catalyst. After stabilization, the test procedure was started at  $25^\circ\text{C}$  followed by increasing the catalyst temperature, at a rate of  $2^\circ\text{C min}^{-1}$ , up to  $500^\circ\text{C}$ . The temperature was maintained for

30 min and then cooled to room temperature at a rate of  $1^\circ\text{C min}^{-1}$ . The reaction products were analyzed by the same apparatus as those used for the NOx reaction tests. All light-off curves presented in this work were obtained during the cooling ramp. The total  $\text{C}_3\text{H}_6$  conversion, the conversion of  $\text{C}_3\text{H}_6$  into  $\text{CO}_2$  and CO and the carbon balance are given by the following Eqs. (4)–(7):

$$X_{\text{C}_3\text{H}_6} = 100 \times \left( 1 - \frac{[\text{C}_3\text{H}_6]_t}{[\text{C}_3\text{H}_6]_{t0}} \right) \quad (4)$$

$$X_{\text{C}_3\text{H}_6-\text{CO}_2} = 100 \times \left( \frac{(1/3)[\text{CO}_2]_t}{[\text{C}_3\text{H}_6]_{t0}} \right) \quad (5)$$

$$X_{\text{C}_3\text{H}_6-\text{CO}} = 100 \times \left( \frac{(1/3)[\text{CO}]_t}{[\text{C}_3\text{H}_6]_{t0}} \right) \quad (6)$$

$$3[\text{C}_3\text{H}_6]_{t0} = 3[\text{C}_3\text{H}_6]_t + [\text{CO}_2]_t + [\text{CO}]_t \quad (7)$$

For information, the adiabatic temperature due to  $\text{C}_3\text{H}_6$  oxidation into  $\text{CO}_2$  and/or CO is given by Eq. (9). In the case of 100%  $\text{C}_3\text{H}_6$  converted into  $\text{CO}_2$  or into CO, the corresponding maximum  $\Delta T$  obtained was approximately 64 and  $14^\circ\text{C}$ , respectively.

$$\Delta T = \frac{\Delta H_r(\text{CO}_2) \times [\text{C}_3\text{H}_6]_0 \times X_{\text{C}_3\text{H}_6/\text{CO}_2}}{10^6 \times C_p} + \frac{\Delta H_r(\text{CO}) \times [\text{C}_3\text{H}_6]_0 \times X_{\text{C}_3\text{H}_6/\text{CO}}}{10^6 \times C_p} \quad (9)$$

With  $\Delta H_r(\text{C}_3\text{H}_6 \text{ into } \text{CO}_2) = 1885.5\text{ kJ mol}^{-1}$ ;  $\Delta H_r(\text{C}_3\text{H}_6 \text{ into } \text{CO}) = 311.2\text{ kJ mol}^{-1}$ ;  $[\text{C}_3\text{H}_6]_0 = 1100\text{ ppm}$ ;  $10^6 = \text{ppm}$  and  $C_p \text{ air} = 32\text{ J kg}^{-1}\text{ K}^{-1}$ .

## 3. Results

### 3.1. Characterizations

#### 3.1.1. Specific surface area and ceria content

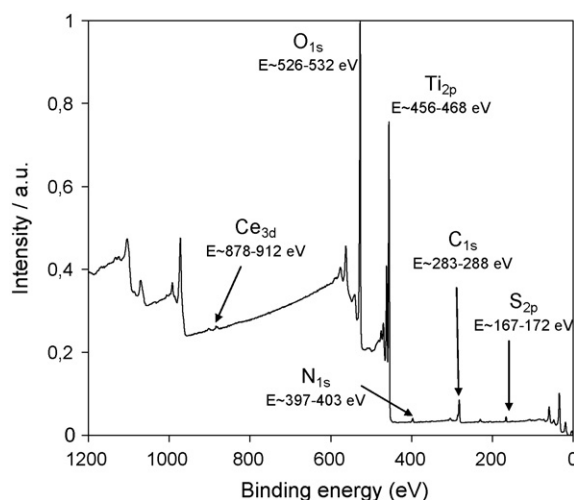
Table 1 summarizes the ceria content of the samples and the  $S_{\text{BET}}$  of the sulphated  $\text{TiO}_2$  support alone and of the catalysts after catalytic testing (previously calcined under dry air at  $500^\circ\text{C}$  for 2 h). The ceria content determined by ICP measurement is close to the theoretical value. Ceria content had only a small impact on the  $S_{\text{BET}}$  compared to the sulphated titania support with a  $S_{\text{BET}}$  of  $121\text{ m}^2\text{ g}^{-1}$ . Furthermore, at the higher the ceria content, the lower the  $S_{\text{BET}}$  value. The highest  $S_{\text{BET}}$  obtained was for the Ce0.04 sample at  $112\text{ m}^2\text{ g}^{-1}$  whereas the lowest  $S_{\text{BET}}$  value was for the Ce0.9 sample at  $106\text{ m}^2\text{ g}^{-1}$ . It can be assumed that ceria fills the pores of the sulphated titania support without modifying the pore shape. This was based on the isotherm patterns for the two catalysts which did not display any differences.

#### 3.1.2. Surface composition

XPS analysis was carried out in order to determine the nature of the different compounds (S, C, N, Ti, O and Ce) and to quantify the sulphur element present at the surface of the different catalysts. The general XPS spectra, recorded between 1200 and 0 eV for Ce0.9 sample, is reported in Fig. 1. The binding energy (BE)

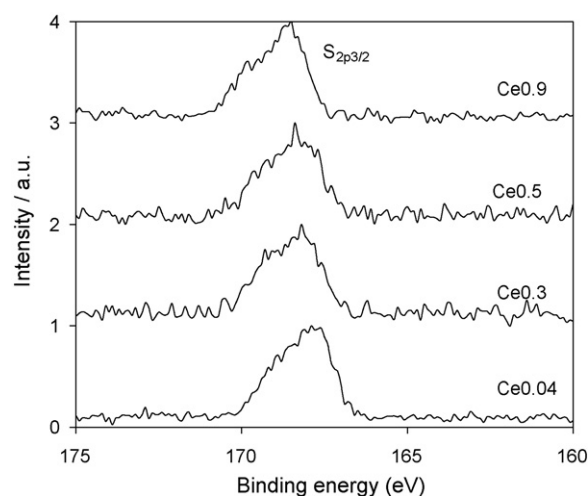
**Table 1**  
Specific surface area and Ce content determined by ICP of the Ce/ $\text{TiO}_2$  sulphated catalyst.

Catalyst composition	Sample name	Ce content/wt%	$S_{\text{BET}}/\text{m}^2\text{ g}^{-1}$
$\text{TiO}_2$ sulphated	–	–	121
Ce(0.04%)/ $\text{TiO}_2$ sulphated	Ce0.04	0.04	112
Ce(0.3%)/ $\text{TiO}_2$ sulphated	Ce0.3	0.30	109
Ce(0.5%)/ $\text{TiO}_2$ sulphated	Ce0.5	0.45	107
Ce(0.9%)/ $\text{TiO}_2$ sulphated	Ce0.9	0.90	106



**Fig. 1.** Overall photoemission spectra for binding energy between 0 and 1200 eV for the Ce0.9 sample.

ranges for the main peaks of the different elements are 167–172 eV for  $S_{2p}$ , 283–288 eV for  $C_{1s}$ , 397–403 eV for  $N_{1s}$ , 456–468 for  $Ti_{2p}$ , 526–532 eV for  $O_{1s}$  and 878–912 eV for  $Ce_{3d}$ . The positions of the main peaks are given in Table 2. For the  $C_{1s}$  band, the peak at 284.6 eV can be ascribed to C graphite (284.3 eV in [18]) and/or C–H bonds (283.9 eV in [19]) and not to interactions between C and Ti (281.6 eV in [20]). Concerning the  $N_{1s}$  peak, the value of 399.8 eV is correlated to  $N_{ads}$  (399.5 eV in [21]), and not due to bonds between N and Ti (396.8 eV in [22]) or between N and C (395.7 eV in [20]). An enlarged image of the  $S_{2p}$  peaks is given in Fig. 2. Concerning the nature of the S species, it was observed that the maximum BE peak of  $S_{2p}$ , between 167.6 and 168.4 eV, was linked to sulphate compounds,  $SO_3^{2-}$  (166.7 eV in [23]) or  $SO_4^{2-}$  (169 eV in [24]), and not due to S from sulphide ( $S^{2-}$ ) (161.2 eV in [25]) or  $S_2O_3^{2-}$  (162.9 eV in [26]). This agrees with the results of Desmartin-Chomel et al. [27] who showed, by FTIR study, that sulphated  $TiO_2$  surface is covered by di-sulphate and/or mono-sulphated species. The di-sulphate species are easily transformed into mono-sulphates by reacting with a strong base like  $NH_3$ . Concerning XPS spectra of ceria, the interpretation of the  $Ce_{3d}$  peaks is not easy due to the presence of more than 10 peaks correlated to multielectronic processes in the  $Ce^{4+}$  and  $Ce^{3+}$  states [28,29]. Thus, only qualitative analysis on the oxidation of ceria was completed. Due to the low ceria content, Ce peaks could be detected only on the Ce0.9 sample. An enlarged image of the  $Ce_{3d}$  peaks is shown in Fig. 3. Firstly, the main  $Ce_{3d_{5/2}}$  peak at 880.8 eV is correlated to the  $Ce_2O_3$  compound (881.5 eV in [30]). The BE correlated to the  $CeO_2$  compound is slightly higher, 882 eV [30]. Moreover, Holgado et al. [31] have demonstrated that the ratio between the  $Ce_{3d_{5/2}}$  peak at 880.8 eV and its satellite at 883.8 eV could give information on the oxida-



**Fig. 2.**  $S(2p)$  photoemission spectra for Ce catalysts.

tion state of Ce. They concluded that if the satellite peak height was greater than the main  $Ce_{3d_{5/2}}$  peak, then  $Ce^{3+}$  is the dominant species in the sample. Secondly, the isolated peak at 916.9 eV was attributed to the presence of  $Ce^{4+}$  state and its intensity related to the amount of  $Ce^{4+}$  ions. For the Ce0.9 sample, the signal correlating to the  $u'''$  peak (nomenclature of Burroughs et al. [32]) was very low and attributed to the presence of  $Ce^{3+}$ . Thus, it was concluded that after (and maybe during)  $C_3H_6$ -SCR, the  $Ce_2O_3$  phase is present at the surface of the catalyst and that  $Ce^{3+}Vo$  (Vo: oxygen vacancy) defects remain at the surface of the crystallites.

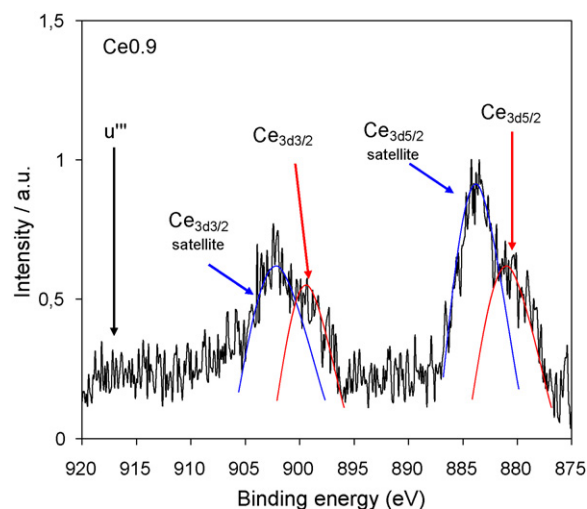
XPS analysis was carried out after ceria impregnation and calcinations to determine the atomic % of the different elements at the surface. The atomic and weight percentages of Ce, Ti and S for the different samples, obtained after reactions, are given in Table 3. Ceria could be detected only on Ce0.9 catalyst, the sample with the highest Ce content. For this catalyst, the experimental weight % of ceria at the surface was 1.1 wt%. This value is close to the overall ceria content determined by ICP analysis, 0.9 wt%. The concentration for S was quantified for all the samples. The S value obtained after ceria impregnation was different from that of the sulphated titania support with a theoretical value of 2 wt% S, and differs between each catalyst. It was observed that ceria impregnation route using aqueous medium and/or calcination treatment modified the stability of the sulphate compound. The Ce0.5 sam-

**Table 2**  
Maximum of the photoemission peaks of O, C, N, Ti, S and Ce elements.

Element	Energy level	Energy binding/eV
O <sup>a</sup>	1s	529.7
C <sup>a</sup>	1s	284.6
N <sup>a</sup>	1s	399.8
Ti <sup>a</sup>	2p <sub>3/2</sub>	457.7–457.8
	2p <sub>1/2</sub>	463.5–463.6
S <sup>a</sup>	2p <sub>3/2</sub>	167.8–168.4
	3d <sub>5/2</sub>	880.8 satellite 883.8
Ce <sup>b</sup>	3d <sub>3/2</sub>	899.3 satellite 902
	$u'''$	916.9

<sup>a</sup> For all catalysts.

<sup>b</sup> Only for Ce0.9 catalyst.



**Fig. 3.** Zoom of  $Ce(3d_{5/2})$  and  $Ce(3d_{3/2})$  photoemission peak for the Ce0.9 catalyst.

**Table 3**Atomic and weight percentage of Ce, Ti and S elements determined by XPS analysis (relative error =  $\pm 5\%$ ).

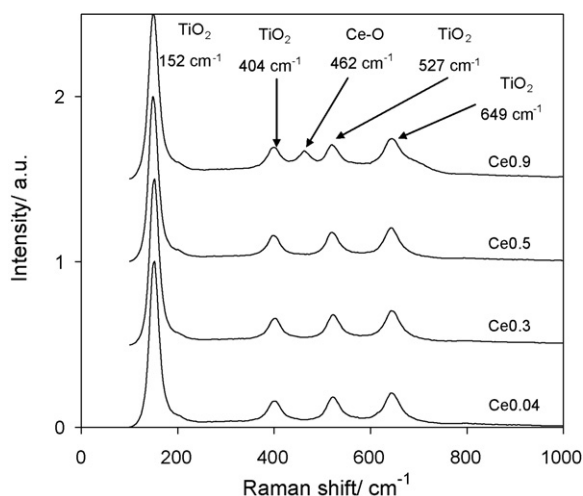
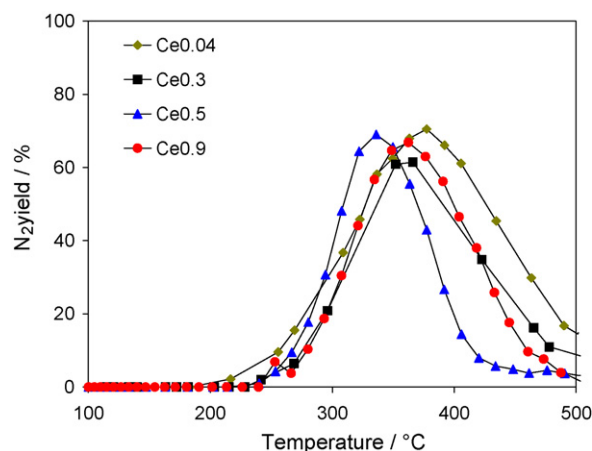
Catalysts	Ce	Ti	S	S/Ti <sup>c</sup>
Ce0.04	n.d. <sup>a</sup>	23.7	0.8 $\leftrightarrow$ 1.1	0.03
Ce0.3	n.d. <sup>a</sup>	24.9	1.0 $\leftrightarrow$ 1.4	0.04
Ce0.5	n.d. <sup>a</sup>	23.3	1.6 $\leftrightarrow$ 2.2	0.07
Ce0.9	0.2 $\leftrightarrow$ 1.1 <sup>b</sup>	23.5	1.3 $\leftrightarrow$ 1.8	0.06

<sup>a</sup> n.d.: not determined.<sup>b</sup> Atomic %  $\leftrightarrow$  weight %.<sup>c</sup> Atomic ratio.

ple displayed the highest S wt% (2.2). The catalysts ranking in terms of S concentration from highest to lowest is as follows: Ce0.5 > Ce0.9 > Ce0.3 > Ce0.04, corresponding to 2.2, 1.8, 1.4 and 1.1 wt% S, respectively.

### 3.1.3. Ceria particle size

In order to evaluate the crystal size of the ceria particles, Raman spectroscopy was carried out. The Raman spectra of the different catalysts are reported in Fig. 4. Firstly, the bands located at 152, 404, 527 and 649  $\text{cm}^{-1}$  refer to the  $\text{TiO}_2$  anatase structure. Lin and Xiaoming showed the same four peaks located at a slightly lower frequency, 147, 397, 515 and 637  $\text{cm}^{-1}$  [33]. Intermediate frequencies were obtained by Fang et al. [34]. This frequency shift could be due to the different sample used for calibration, the spectral resolution and the size of the particle: the lower the size, the higher the energy (i.e. nanoparticles shift peaks at low frequency values due to oxygen framework stabilization). Secondly, a band at 462  $\text{cm}^{-1}$  was observed only for the Ce0.9 catalyst. It is known that  $\text{CeO}_2$  nanoparticles present a strong band at 457  $\text{cm}^{-1}$  due to the  $\text{F}_{2g}$  Raman active mode of the fluorine structure [35]. This band is assigned to ceria particles. This band is characteristic of the  $\text{CeO}_2$  mode which is linked to the Ce-O8 vibration (fluorine structure) [36]. For the other experimental catalysts, the ceria content was too low to obtain a Raman signal. Many Raman studies have been done in order to correlate Raman signal and ceria structure. Some authors found relations between the half-width of the Raman peak at 465  $\text{cm}^{-1}$  with the ceria particle sizes. The confirmation of the ceria particle sizes was obtained by complementary characterisation methods [37,38]. In this work, the half-width of the peak at 462  $\text{cm}^{-1}$  for the Ce0.9 sample was about 24  $\text{cm}^{-1}$ . The use of the linear equation obtained by Kosachi et al. [38],  $H(\text{cm}^{-1}) = 10 + 124.7/d(\text{nm})$ , calculates the average value for ceria particle size to be 9 nm. However, when the linear equation of

**Fig. 4.** Raman spectra of the Ce based catalysts.**Fig. 5.**  $\text{N}_2$  yield for Ce catalysts during  $\text{NO}_x$  reduction reaction.

Graham et al. [37],  $H(\text{cm}^{-1}) = 10 + 436/d(\text{\AA})$  was adopted, a lower value, around 2.5 nm was calculated. Both results are in opposition with those obtained by Wang et al. [39]. Indeed, in this study, the presence of small ceria particles ( $d_p < 17$  nm) would involve the apparition in the Raman spectra of two bands located at 270 and 315  $\text{cm}^{-1}$ . The Ce0.9 sample did not reveal these bands thus in this last case the ceria particle size should be above 17 nm. Hence, no information could be obtained on the ceria particle size.

### 3.1.4. Characterization summary

To conclude on the sample characterization, ceria had a slight inhibitor effect on the surface area and the presence of  $\text{Ce}^{3+}$  cation was observed on the catalyst surface. The Ce cation species provided sites for oxygen vacancies and the presence of sulphated species such as  $\text{SO}_3^{2-}$  or  $\text{SO}_4^{2-}$  anions. However, no clear indication could be obtained on the ceria particle size.

## 3.2. NO reduction test

In order to evaluate the selective catalytic reduction of NO by  $\text{C}_3\text{H}_6$  over the ceria/sulphated titania catalysts, NO reduction tests were carried out. In this study, results were focused only on the NO conversion into  $\text{N}_2$ ,  $\text{N}_2$  selectivity, and total  $\text{C}_3\text{H}_6$  conversion. The evolution of  $\text{NO}_2$  and  $\text{N}_2\text{O}$  products are not presented here. However, for all the samples, the  $\text{NO}_2$  production occurred at temperatures higher than 400  $^\circ\text{C}$  and did not exceed 20% at 500  $^\circ\text{C}$  (maximum obtained for Ce0.5 sample), whereas  $\text{N}_2\text{O}$  was not detected in the temperature range studied, between 25 and 500  $^\circ\text{C}$ . For each experiment the nitrogen balance, including NO,  $\text{N}_2$ ,  $\text{NO}_2$  and  $\text{N}_2\text{O}$ , was checked.

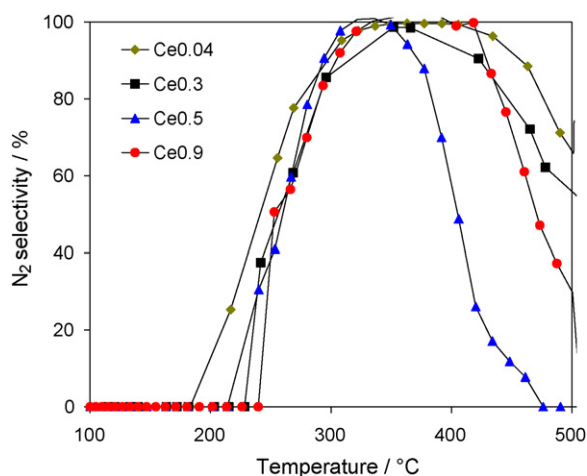
Firstly, all the catalysts show a volcano shaped plot for the  $\text{N}_2$  yield which tends to decrease to zero at temperatures above 500  $^\circ\text{C}$  as reported in Fig. 5. Table 4 summarizes the maximum conversion rate of NO to  $\text{N}_2$  and the corresponding temperature. Concerning the maximum conversion, two groups of catalysts can be identified: (i) Ce0.3 sample with a maximum of 61 and (ii) Ce0.04, Ce0.5 and Ce0.9 samples with a maximum of 70, 69 and 67%, respectively. However, even though the profile curves are similar, the Ce0.5 sample displayed the lowest temperature for the maximum conversion, 336  $^\circ\text{C}$ . Table 4 presents the maximum  $\text{N}_2$  selectivity and the temperature window for a  $\text{N}_2$  selectivity of 80%. The variations of  $\text{N}_2$  selectivity with the reaction temperature are presented in Fig. 6. Below 335  $^\circ\text{C}$ , all the catalysts display the same curve shape, with a fast increase above 200  $^\circ\text{C}$ , up to 100%. For temperatures higher than 335  $^\circ\text{C}$ , the Ce0.04, Ce0.3 and Ce0.9 samples are more selective towards  $\text{N}_2$



**Table 4**

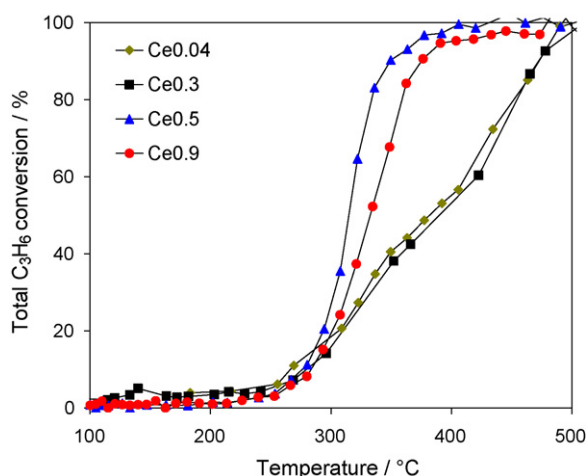
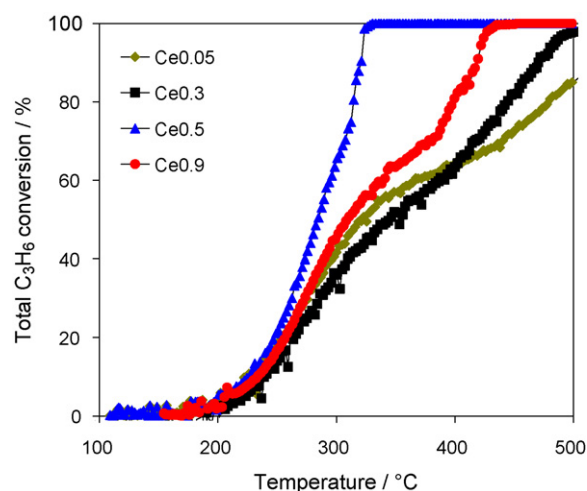
NOx reduction reaction data for Ce catalysts.

Catalyst	Conversion NO–N <sub>2</sub>		N <sub>2</sub> selectivity		Total C <sub>3</sub> H <sub>6</sub> conversion		
	Max/%	T <sub>max</sub> /°C	Max/%	Window T <sub>80</sub> /°C	T <sub>ignition</sub> /°C	T <sub>50</sub> /°C	T <sub>100</sub> /°C
Ce0.04	70	377	100	270–475	216	378	500
Ce0.3	61	367	100	290–447	216	390	500
Ce0.5	69	336	100	280–377	214	310	405
Ce0.9	67	362	100	290–435	226	336	420

**Fig. 6.** N<sub>2</sub> selectivity for Ce catalysts during NOx reduction reaction.

than the Ce0.5 sample. In addition, the N<sub>2</sub> selectivity windows (80%) were larger ( $\Delta T > 150^\circ\text{C}$ ) for Ce0.5 sample ( $\Delta T = 100^\circ\text{C}$ ) than for these last catalysts. The Ce0.5 catalyst had a similar maximum N<sub>2</sub> yield of 69% but it had the lowest N<sub>2</sub> selectivity window.

Finally, the total conversion of C<sub>3</sub>H<sub>6</sub> is shown in Fig. 7. Table 4 summarizes the temperature of C<sub>3</sub>H<sub>6</sub> ignition and the temperature for 50 and 100% of C<sub>3</sub>H<sub>6</sub> conversion. The temperature of ignition was similar for all the catalysts, starting around 220°C. However, for temperatures higher than 300°C, the Ce0.5 and Ce0.9 samples were the most active catalysts with a T<sub>50</sub> of 310 and 336°C, respectively and both reached a conversion of 100% for C<sub>3</sub>H<sub>6</sub> at 410°C. By contrast, the Ce0.3 and Ce0.04 catalysts presented a T<sub>50</sub> of 390 and 378°C, respectively and reached a conversion of 100% at 500°C.

**Fig. 7.** Total C<sub>3</sub>H<sub>6</sub> conversion for Ce catalysts during NOx reduction reaction.**Fig. 8.** Total C<sub>3</sub>H<sub>6</sub> conversion for Ce catalysts during propene oxidation reaction.

### 3.3. C<sub>3</sub>H<sub>6</sub> oxidation test

The catalytic properties of the ceria/sulphated titania compounds for propene oxidation were evaluated separately. The curves for total C<sub>3</sub>H<sub>6</sub> oxidation are presented in Fig. 8. The ignition temperature and the temperature for 50 and 100% conversion of C<sub>3</sub>H<sub>6</sub> are given in Table 6. The ceria content did not affect the ignition of propene oxidation. All the catalysts had ignition temperatures around 195°C. The lowest light-off temperature was obtained for the Ce0.5 sample where T<sub>50</sub> equalled 284°C. Ranking the catalyst based on T<sub>50</sub> order from lowest to highest is as follows: Ce0.5 > Ce0.9 > Ce0.04 > Ce0.3. However, for temperature higher than 400°C, the conversion order follows the ceria content. The sample with 0.5 wt% of Ce was observed to have the best catalytic behaviour in the propene oxidation reaction.

Arrhenius plots,  $\ln(X_{\text{C}_3\text{H}_6}) = f(1/T)$  for  $X_{\text{C}_3\text{H}_6} < 0.2$ , are shown in Fig. 9 and the corresponding values for the activation energy (E<sub>a</sub>) are summarized in Table 5. The Ce0.5 sample had the lowest E<sub>a</sub> with a value of 60 kJ mol<sup>−1</sup>. The highest E<sub>a</sub> value was obtained for the Ce0.3 sample, 82 kJ mol<sup>−1</sup>. It is important to notice that for all the ceria catalysts, the analysis of the products during C<sub>3</sub>H<sub>6</sub> oxidation revealed only the presence of CO<sub>2</sub> and CO. For Ce0.3 sample, in Fig. 10, the carbon balance evaluated by the sum of (CO + CO<sub>2</sub>) was equivalent to the total C<sub>3</sub>H<sub>6</sub> consumption within experimental error (±5%). For this sample, two reaction pathways can be sug-

**Table 5**Activation energy (E<sub>a</sub>), T<sub>initial</sub>, T<sub>50</sub> and T<sub>100</sub> for total C<sub>3</sub>H<sub>6</sub> oxidation of the Ce/TiO<sub>2</sub> sulphated catalyst obtained during propene oxidation reaction.

Catalyst	E <sub>a</sub> /kJ mol <sup>−1</sup>	Total C <sub>3</sub> H <sub>6</sub> conversion		
		T <sub>ignition</sub> /°C	T <sub>50</sub> /°C	T <sub>100</sub> /°C
Ce0.04	66	190	321	–
Ce0.3	82	200	345	500
Ce0.5	60	193	284	328
Ce0.9	65	194	309	440

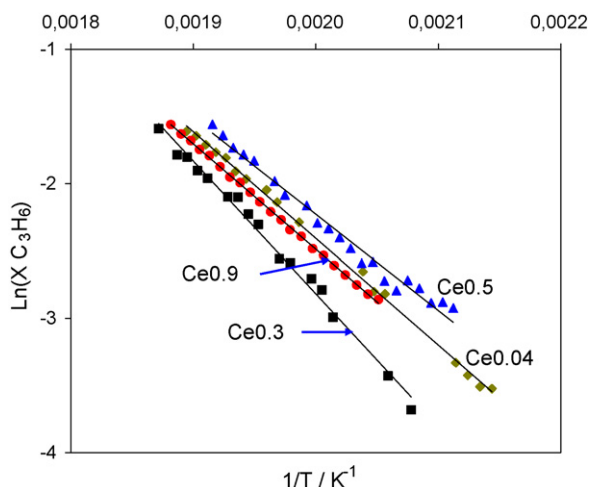


Fig. 9. Arrhenius plot for Ce catalysts obtained after propene oxidation reaction.

gested from this observation. In the first pathway,  $C_3H_6$  is converted to CO, followed by CO oxidation to form  $CO_2$  while in the second pathway, CO and  $CO_2$  are simultaneously produced. For the studied catalysts here, the second pathway was confirmed involving two reaction sites. In the temperature range studied, 100–500 °C, two distinct reaction domains appear. The first reaction domain for Ce0.3 sample is observed in the temperature range of 100–380 °C, while the second reaction domain occurs between 380 and 500 °C. In the first reaction domain, the production of CO and  $CO_2$  increased simultaneously. The partial and total propene oxidation to CO and  $CO_2$  occurred. In the second temperature range, CO conversion decreased while  $CO_2$  production continued to increase. The  $CO_2$  enhancement can be due to the total propene oxidation or the thermal oxidation of CO in the gas phase. However, in order to achieve the simultaneous production of CO and  $CO_2$  two surface reaction sites must be involved. At this stage, it is difficult to characterize such active sites presenting different interactions between ceria, titania, and sulphate compounds.

### 3.4. Discussion

The  $C_3H_6$ -SCR of NO and the  $C_3H_6$  oxidation tests were carried out in order to find a correlation between selective catalytic reduction of NOx, partial  $C_3H_6$  oxidation and sulphate content.

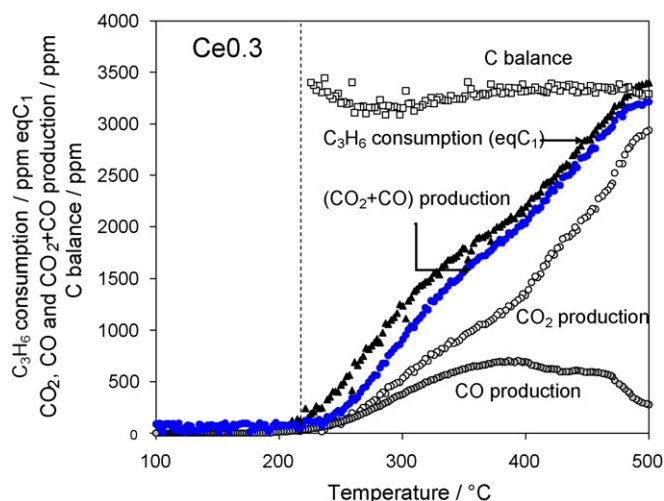


Fig. 10.  $C_3H_6$  consumption,  $CO_2$  and CO production and C balance for Ce0.3 sample during propene oxidation reaction.

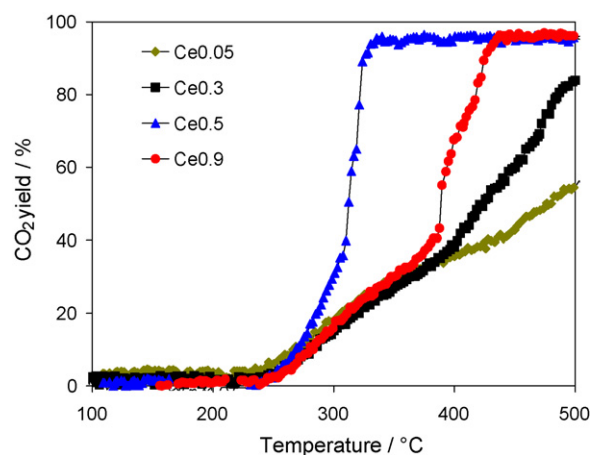


Fig. 11. Conversion of  $C_3H_6$  into  $CO_2$  for Ce catalysts during propene oxidation reaction.

The conversion of  $C_3H_6$  into  $CO_2$  obtained during the  $C_3H_6$  oxidation test is shown in Fig. 11. The ignition temperature and the temperatures where 50 and 100% conversion of  $C_3H_6$  into  $CO_2$  was observed, and the fraction value of propene partially oxidized to CO at 300, 350, 400, 450 and 500 °C are summarized in Table 6. The partial oxidation ratio ( $R_{PO}$ ) represents the fraction of  $C_3H_6$  oxidised into CO and is defined by the following Eq. (8) and presented in Fig. 12:

$$R_{PO} = 1 - \frac{(n_{C_3H_6/CO_2})_t}{(n_{C_3H_6})_{t0}} = \frac{(n_{C_3H_6/CO})_t}{(n_{C_3H_6})_{t0}} \quad (8)$$

The Ce0.5 sample was observed to have the highest total  $C_3H_6$  conversion to  $CO_2$  (i.e. the lowest CO production). Furthermore, the  $T_{50}$  for the Ce0.5 sample was close to 310 °C while the second most active catalyst, Ce0.9, was observed to have  $T_{50}$  at 387 °C. The catalyst ranking based on the  $R_{PO}$  from lowest to highest is Ce0.04 > Ce0.3 > Ce0.9 > Ce0.5. The same order was observed for  $N_2$  selectivity. However, the inverse order was observed for  $C_3H_6$  oxidation in the absence of NO,  $C_3H_6$  oxidation with NO ( $C_3H_6$ -SCR conditions) and NOx activity, Ce0.04 < Ce0.3 < Ce0.9 < Ce0.5. The correlating factor between all these properties seems to be the S wt% content: Ce0.5 > Ce0.9 > Ce0.3 > Ce0.04. Thus, the process occurring during the NOx reduction by  $C_3H_6$  seems to be represented by two main steps: (i) at lower temperatures, ~240 °C, the acidity of the support, due to the presence of S compounds, ini-

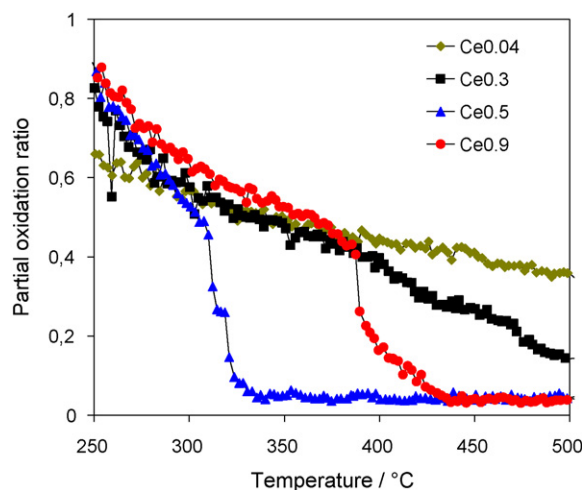


Fig. 12. Partial oxidation ratio of Ce catalysts obtained after propene oxidation reaction.

**Table 6**C<sub>3</sub>H<sub>6</sub> oxidation reaction data for Ce catalysts.

	Conversion C <sub>3</sub> H <sub>6</sub> –CO <sub>2</sub>				Partial oxidation ratio ( <i>R</i> <sub>OP</sub> )				
	<i>T</i> <sub>ignition</sub> /°C	<i>T</i> <sub>50</sub> /°C	Max/%	<i>T</i> <sub>max</sub> /°C	300	350	400	450	500
Ce0.04	190	476	54	496	0.57	0.50	0.43	0.40	0.36
Ce0.3	200	424	84	500	0.61	0.47	0.40	0.27	0.14
Ce0.5	193	312	96	335	0.53	0.05			
Ce0.9	194	387	96	434	0.65	0.53	0.16	0.4	

tiates the NO<sub>x</sub> reduction. The S concentration did not seem to influence the ignition temperature. (ii) At higher temperatures, when the reduction process is ignited, the S wt% has a role on the NO<sub>x</sub> reduction activity and the higher the S concentration, the higher the CO<sub>2</sub> yield was. This higher total C<sub>3</sub>H<sub>6</sub> oxidation into CO<sub>2</sub> decreased the catalyst activity toward N<sub>2</sub> yield, and subsequently, decreased the N<sub>2</sub> selectivity. In the literature, a deeper characterization of the acid-catalyzed process provides a better understanding of the C<sub>3</sub>H<sub>6</sub>–SCR mechanism over Ce/TiO<sub>2</sub> sulphated catalysts. The mechanism begins in the presence of reduced ceria which provides a surface for the formation of nitrate (NO<sub>3</sub><sup>−</sup>) by means of NO<sup>−</sup>, N<sub>2</sub>O and a dissociation product. However, in parallel, a second minor process could occur where reduced ceria is reoxidized by NO<sup>−</sup> formation or NO dissociation, leading to immediate and thermal N<sub>2</sub> desorption [40]. Nitrates can be formed on sulphated TiO<sub>2</sub> surface by the reaction of NO<sup>−</sup> on bi- or mono-sulphated species: NO<sup>−</sup> + 2SO<sub>4</sub><sup>2−</sup> → NO<sub>3</sub><sup>−</sup> + 2SO<sub>3</sub><sup>2−</sup> and/or NO<sup>−</sup> + SO<sub>4</sub><sup>2−</sup> → NO<sub>2</sub><sup>−</sup> + SO<sub>3</sub><sup>2−</sup> [41]. NO<sup>−</sup> species are rapidly oxidized and are less stable on sulphated supports than on pure oxides. In the C<sub>3</sub>H<sub>6</sub>–SCR tests, C<sub>3</sub>H<sub>6</sub> reacted with nitrate species to form acetaldehyde intermediate compounds. NO and O<sub>2</sub>, from the gas mixture, react quickly with carbonyl compounds to form –CN and –NCO species [17]. As remarked earlier, the partial C<sub>3</sub>H<sub>6</sub> oxidation property (*R*<sub>PO</sub>) could predict the formation of some intermediate species, like carbonyls (=CO) that are involved in the formation of acetaldehyde (CH<sub>3</sub>CHO). NCO is hydrolyzed by water produced in the reaction to form –NH complexes that are then transformed into NH<sub>3</sub> [17]. Finally, a reaction between NH<sub>3</sub> and NO occurs to form N<sub>2</sub>. In this bi-functional mechanism, a good activity predictor for N<sub>2</sub> was linked to the number of acid sites, which are the active catalytic sites in C<sub>3</sub>H<sub>6</sub>–SCR reaction [16,42]. The N<sub>2</sub> selectivity was concluded to be related to the partial C<sub>3</sub>H<sub>6</sub> oxidation property (i.e. to the lower wt% S content).

#### 4. Conclusion

In this study, NO<sub>x</sub> reduction activity evaluated by C<sub>3</sub>H<sub>6</sub>–SCR over different ceria/sulphated TiO<sub>2</sub> catalysts (ceria content of 0.9, 0.5, 0.3 and 0.04 wt%) was related to the partial C<sub>3</sub>H<sub>6</sub> oxidation and the S content. The NO<sub>x</sub> abatement activity was not correlated to the ceria content, but correlated to the sulphate content. The higher the sulphate content, the higher the NO<sub>x</sub> activity. Moreover, this activity was linked to the partial C<sub>3</sub>H<sub>6</sub> oxidation activity. The lower the partial C<sub>3</sub>H<sub>6</sub> oxidation was, the better the NO<sub>x</sub> activity was. Nevertheless, the N<sub>2</sub> selectivity was better for the catalyst containing the lowest sulphate content (i.e. the best partial C<sub>3</sub>H<sub>6</sub> oxidation). Sulphate compounds like SO<sub>3</sub><sup>2−</sup> and/or SO<sub>4</sub><sup>2−</sup> and reduced ceria have to activate C<sub>3</sub>H<sub>6</sub> and NO compounds. In a second stage, in the range of ceria content studied here, the presence of NO or not, propene oxidation was not linked to ceria content but was related to sulphate content. However, the presence of Ce<sup>3+</sup>/Vo species, involving O vacancies, could provide oxygen for NO oxidation yielding nitrate. To conclude, the sulphate content was observed to be the key parameter in NO<sub>x</sub> reduction and N<sub>2</sub> selectivity.

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